

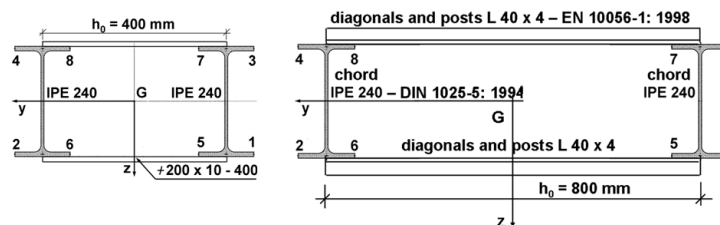
## Analysis of metal built-up members

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Battened built-up member. The analysis of the 2<sup>nd</sup> order with imperfection is used in calculations. The geometrical equivalent global initial sway imperfection is taken according to EN 1993-1-1. The column is made of steel S355. The yield strength  $f_y = 355$  MPa, the safety factors  $\gamma_{M0} = 1.0$ ,  $\gamma_{M1} = 1.0$ . The member cross-section is given in Fig. 1.



a) battened built-up member      b) laced built-up member  
 Fig. 1. Cross-section of the built-up columns 2 IPE 240 – DIN 1025-5: 1994

The design values of the external actions applied at the column top with the length  $L = 7.2$  m are given in Fig. 2 together with the obtained results of the analytical analysis. The horizontal force  $H_{Ed,tot}$  consists of two parts: the external force  $H_{Ed} = 22$  kN and the replacement of the global initial sway imperfection by equivalent horizontal force  $N_{Ed}\Phi = 850$  kN / 268.328 = 3.205 kN.

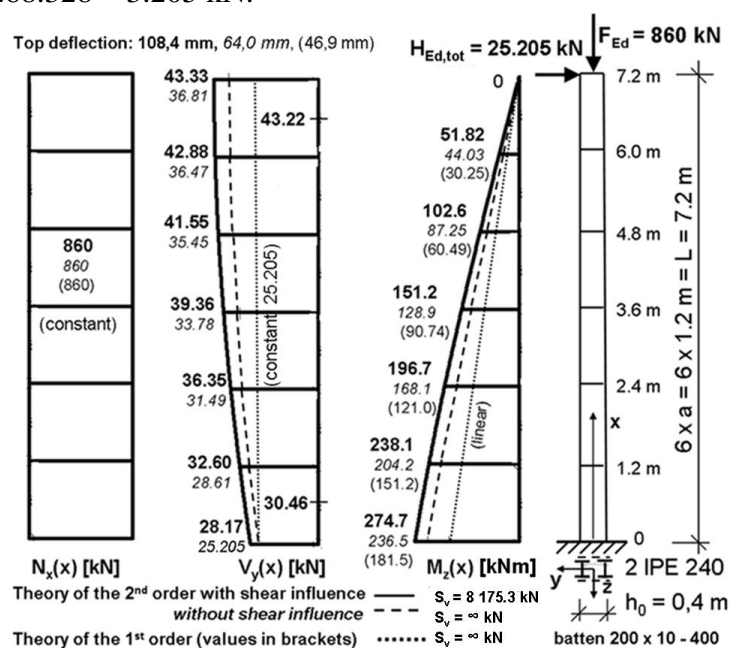


Fig. 2. Column geometry, actions and distributions of the internal forces  $N_x(x)$ ,  $V_y(x)$ ,  $M_z(x)$

Laced built-up member. The cross-section is in Fig. 1 b). The design values of the external actions applied at the column top with the length  $L = 7.2$  m are given in Fig. 3 together with the obtained results of the analytical analysis.

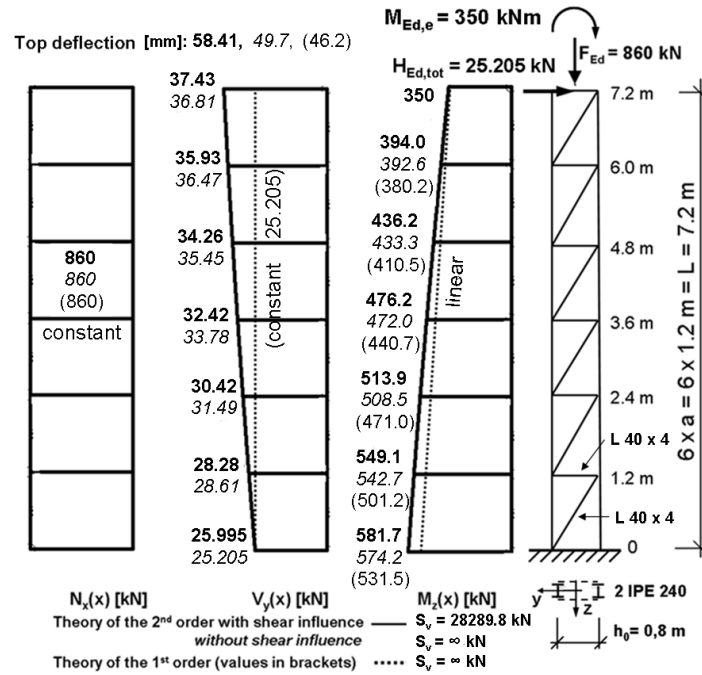


Fig. 3. Column geometry, actions and distributions of the internal forces  $N_x(x)$ ,  $V_y(x)$ ,  $M_z(x)$

Conclusions. The most important parameters of the member are: the shear parameter  $\gamma$ , the member parameter  $\varepsilon$ , the parameter  $\alpha_{cr}$  and amplification factor  $k_{II}$  ( $M_{II} = k_{II} M_I$ ), see Table 1.

Table 1. Shear parameter  $\gamma$ , member parameter  $\varepsilon$ ,  $\alpha_c$  and amplification factor  $k_{II}$ . Index V indicates shear effects

Member parameters	Battened built-up member	Laced built-up member
$\gamma = [1 / (1 - N_{Ed} / S_V)]^{0.5}$	1.118 (1.0 without shear influence)	1.031 (1.0 without shear influence)
$\varepsilon = L [\gamma N_{Ed} / (EI_{eff})]^{0.5}$	0.863	0.418
$\alpha_{cr,V} = N_{cr,V} / N_{Ed}$	3.702 (for $N_{cr,V}$ ); 2.664 (for $N_{cr}$ )	14.542 (for $N_{cr,V}$ ); 10.084 (for $N_{cr}$ )
$k_{II,V} \approx \alpha_{cr,V} / (\alpha_{cr,V} - 1)$	1.370 (for $N_{cr,V}$ ); 1.601 (for $N_{cr}$ )	1.074 (for $N_{cr,V}$ ); 1.110 (for $N_{cr}$ )
by calculation: $k_{II,V} = M_{II,V} / M_I$	$274.7 / 181.5 = 1.513$	$581.7 / 531.5 = 1.094$

Notes: These parameters give to the designer information about built-up members without doing calculations similar to those in Figs. 2 and 3. More details including analytical solutions and Eurocode EN 1993-1-1 verification conditions may be found in [2, 3]. The comparisons of the results of the analytical solutions given in Figs. 2 and 3 with the results of the computer program IQ 100 [4] shown zero differences. The calculations according to the former Czechoslovak standard STN 73 1401: 1968 are in [1].

## Acknowledgements

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