

A new ZVT multi input converter for hybrid sources systems

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Abstract – Renewable energy sources such as wind and solar energy sources are unreliable in different weather conditions to provide constant output voltage. So the concurrent use of different input sources is inevitable to provide a constant load. The use of a Multi-Input Converters (MICs) instead of several separate converters can reduce the number of passive elements. Also it can save the cost and reduce the weight and the volume of the converter. In this paper, a Zero Voltage Transition (ZVT) dual input boost converter is proposed. In addition to the mentioned advantages for the multi-input converters, in the proposed converter only one auxiliary circuit is used for providing soft switching condition for all semiconductor elements and increasing the efficiency. The proposed converter theoretically is analyzed. Then, in order to show the validity of theoretical analysis, it is simulated by ORCAD. The simulation results confirmed the theoretical analysis. The efficiency comparison shows one percent improvement in comparison with hard switching counterpart.

Keywords-Hybrid Power Supply, Multi Input Converter (MIC), Zero Voltage Switching, ZVT

I. INTRODUCTION

Global warming and fuel crisis are important factors for more attention in renewable energy sources [1]-[3]. Wind and photovoltaic energy have capability to supply demand energy in distant places or out of grid and even in densely populated areas. Since the power produced in renewable energy sources are dependent on environmental conditions such as climate and different seasons, concurrent use with other sources is inevitable to ensure the proper operation.

Several independent converters or a multi input converter can be used to supply the load from several distinct sources. The idea of multi input converters originated from combination of independent converters to make high power converters [4],[5]. By using a multi input converter, the cost of semiconductor and passive elements is reduced. For example, one output filter can be used for several converters. Therefore, it reduces the size and increases the efficiency of the converter. Also another advantage

of MICs is possibility of easier control, higher flexibility and better management in energy sources.

MICs divide into two categories including Magnetically Coupled Converter (MCC) and Electrically Coupled Converter (ECC) [6]-[10]. ECCs have the advantages such as high reliability and easier control in variable input Compared to the MCCs But, they have the disadvantages like non-isolation between input and output and non-multilevel output.

Generally, the main purposes of designer are improving efficiency, reliability and reducing the cost of system. Therefore, different topologies for MICs have been proposed in recent years. To achieve above objectives, soft switching technique has been used. Because it can reduce the switching losses and Electromagnetic Interference (EMI) [11],[12].

In [13],[14] tried to provide soft switching and increase the efficiency condition for all of switches simultaneously only by adding one auxiliary circuit. But the main problem of presented topologies in these references are that only soft switching condition is provided for main switches and soft switching condition is not provided for auxiliary switch.

In this paper, a multi input converter for simultaneous or independent use of wind or solar energy resources is presented. In that, the proposed converter provided soft switching for all semiconductor elements simultaneously with only one auxiliary circuit.

In the next section, the performance of the proposed converter is investigated theoretically. The proposed converter is designed at 300 watts. Then the converter performance results are compared with theoretical analysis. Finally, section IV presents the conclusions.

II. PROPOSED CONVERTER

The proposed dual input converter is shown in the fig. 1. The general structure of the proposed converter consists of two boost converter with one auxiliary cell that provides zero voltage soft switching condition for both converters. The auxiliary circuit is shown in the dotted box. The proposed converter can work with one

source independently or with two input sources simultaneously.

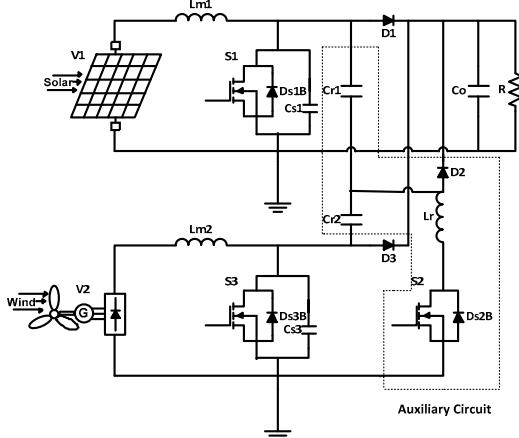


Figure 1. The proposed ZVT dual input converter

In order to analyze the proposed converter in the steady state and during a switching cycle, the following assumptions are made. The output capacitor C_o and input inductors (L_{m1} , L_{m2}) are assumed to be large enough so they can be considered an ideal DC voltage and current source respectively. All of the circuit elements are ideal and the converter is operated in continuous Current Mode CCM.

The operation of this circuit is analyzed in ten modes. To control the converter, the two main switches turn on simultaneously, but may turn off asynchronously. Equivalent circuit of each mode is shown in fig. 3. Also in fig. 2 key waveform of the theoretical analysis is shown. Before the first mode, all of the semiconductor devices instead of D_1 and D_3 are off. Also the voltage of C_{r1} and C_{r2} and current of L_r are zero.

Mode 1 [t_0-t_1] The auxiliary switch S_2 turns on at t_0 under ZC condition. A resonance occurs between L_r , C_{r1} and C_{r2} . This mode continues until current of L_r reaches the output current. The current of L_r and the voltage of C_r are expressed by the following equations.

$$I_{Lr} = \frac{V_0}{Z_1} \sin(\omega_l(t - t_0)) \quad (1)$$

$$V_{cr}(t) = V_0 - V_0 \cos(\omega_l(t - t_0)) \quad (2)$$

$$Z_1 = \sqrt{\frac{L_r}{C_r}} \quad (3)$$

$$C_r = C_{r1} + C_{r2} \quad (4)$$

$$\omega_l = \frac{1}{\sqrt{L_r C_r}} \quad (5)$$

Mode 2 [t_1-t_2] At the beginning of this mode, D_1 and D_3 are turned off under zero current and voltage condition. Then a resonance between L_r , C_{r1} , C_{r2} , C_{s1} and C_{s3} is started. This state continues until switch voltage is reached to zero.

Mode 3 [t_2-t_3] At the beginning of this mode C_s is completely discharged and the body diode S_1 and S_3 are turned on. Therefore, S_1 and S_3 can be turned on under zero voltage zero current (ZVZC) condition. Also L_r voltage is equal to $-V_{cr}$. It must be noted that, S_1 and S_3 should be turned on before turning off D_{s1B}

and D_{s3B} . So, I_{Lr} is decreased to I_{in} . In this mode, growth rate of I_{s1} and I_{s3} is determined by the resonant frequency. I_{Lr} and V_{cr} are expressed by the following equations.

$$I_{Lr}(t) = I_2 \cos(\omega_l(t - t_2)) - \frac{V_2}{V_1} \sin(\omega_l(t - t_2)) \quad (6)$$

$$V_{cr}(t) = V_2 \cos(\omega_l(t - t_2)) + I_2 Z_r \sin(\omega_l(t - t_2)) \quad (7)$$

$$I_2 = I_{Lr}(t_2) = \sqrt{\frac{L_r I_{Lr}^2 - C_r V_2^2}{L_r}} \quad (8)$$

$$V_2 = V_{cr}(t_2) = \frac{I_{in}}{C_r} (t_2 - t_1) + \frac{C_s}{C_r} V_o + V_{cr}(t_1) \quad (9)$$

Mode 4 [t_3-t_4] When I_{s3} and I_{s1} are increased to I_{in2} and I_{in1} , this mode is started and D_{s2B} is turned on. Therefore, the auxiliary switch S_2 can be turned off under ZVZC condition. I_{Lr} becomes zero and the C_r voltage reaches to $V_{cr,p}$. D_2 Voltage stress is equal to $V_o + V_{cr,p}$, which $V_{cr,p}$ is shown by (10). Resonance between C_r and L_r continues through S_1 , S_3 and D_{s2B} . Also, the current spike of turning on main switches expressed by (11).

$$V_{cr,p} = \sqrt{\frac{L_r I_{Lr}(t_2)^2 + C_r V_{cr}(t_2)^2}{C_r}} \quad (10)$$

$$I_{st,p} = I_{in} + I_{Lr,p} \quad (11)$$

Mode 5 [t_4-t_5] The resonance stops when the S_2 body diode turns off, at t_4 . This mode is similar to the input inductor charging mode of conventional boost converter.

Mode 6 [t_5-t_6] By turning off the S_3 , V_{cs3} which is equal to switch voltage, linearly charges by I_{in2} . So the S_3 is turned off under ZV condition.

$$V_{cs3} = \frac{(t_6 - t_5)}{C_{s3}} I_{in2} \quad (12)$$

Mode 7 [t_6-t_7] When V_{cs3} reaches to the $V_o - V_{cr,p}$, D_2 is turned on under ZVS condition. This mode continues until C_{r2} is completely discharged and C_{s3} and C_{r1} are charged to reach V_o .

Mode 8 [t_7-t_8] D_3 turns on at t_7 . Then I_{in2} flows through D_3 to the output and D_2 turns off under ZV condition.

Mode 9 [t_8-t_9] By turning off the S_1 , V_{cs1} which is equal to switch voltage, linearly charges by I_{in1} . This mode continues to discharge C_{r1} .

Mode 10 [t_9-t_{10}] This mode is started by turning on D_1 . It is similar to the power transfer state in the conventional boost converter. This mode last until the next switching cycle.

III. SIMULATION RESULTS

The proposed multi input converter has designed based on previous section and for following conditions. Input voltage $V_{in1}=50$ V_{DC}, $V_{in2}=100$ V_{DC}, output power = 300 Watt, output voltage = 200 V_{DC} and the switching frequency is 100 KHz

Based on above specifications, the following circuit elements values are selected as $L_r=5$ uH, $L_{m1}=L_{m2}=1$ mH, $C_{r1}=C_{r2}=15$ nF, $C_{s1}=C_{s2}=1$ nF and

$C_o=100\mu F$. Then the proposed converter is simulated

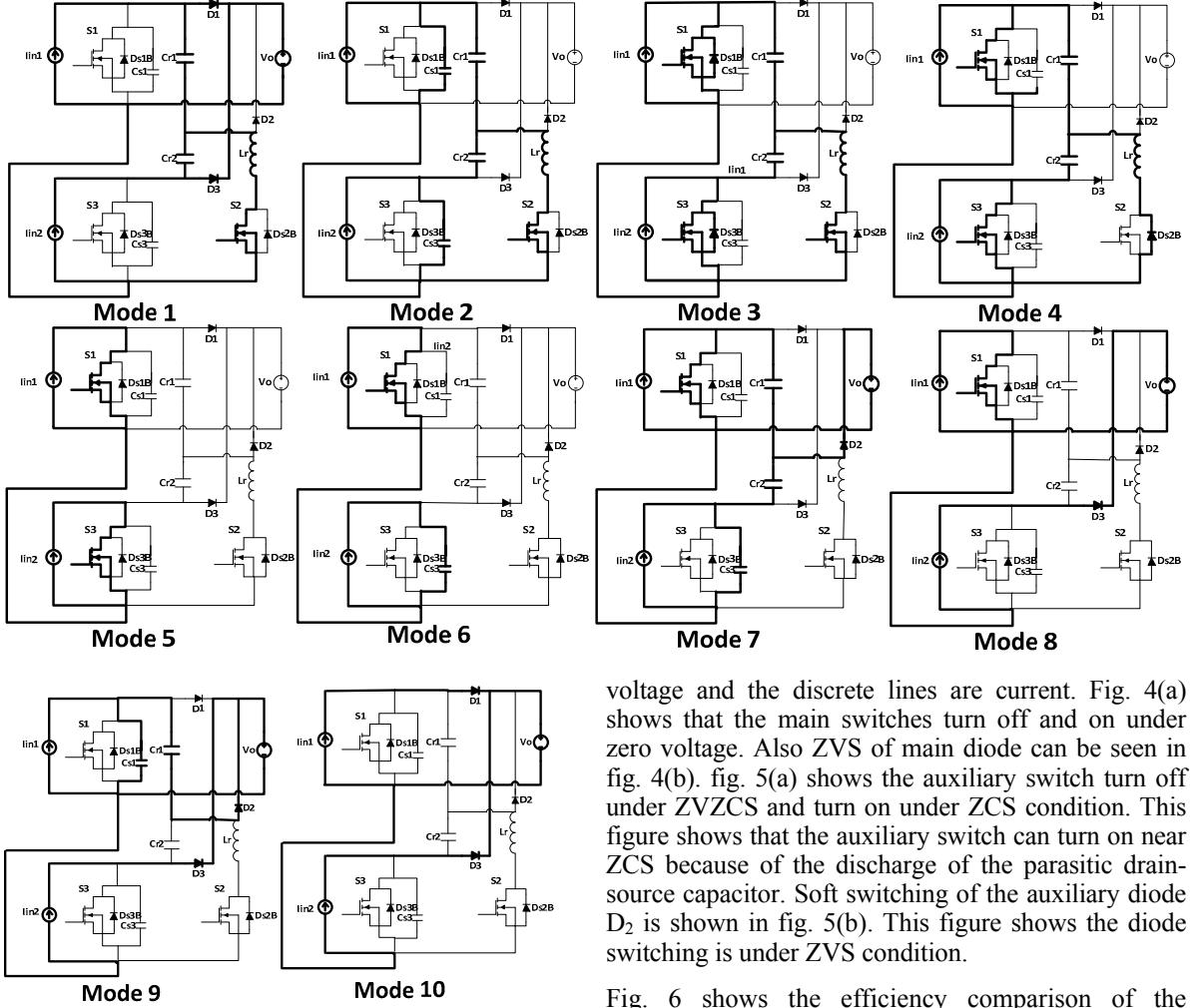


Figure 2. Equivalent circuit during one switching cycle

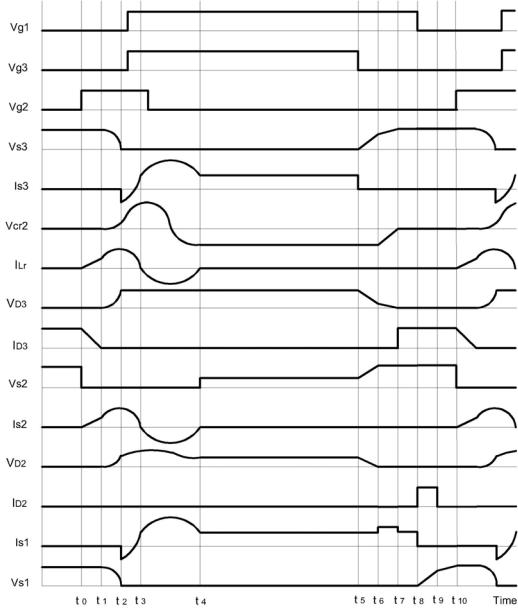
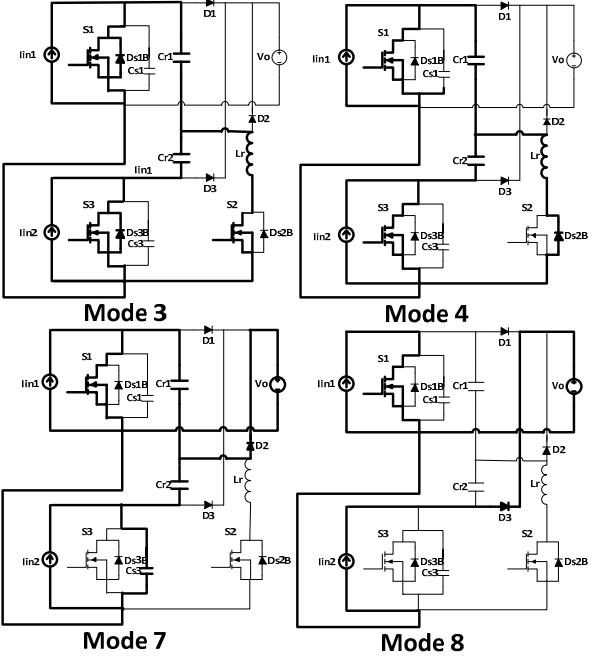


Figure 3. key waveform of the proposed converte

Simulated waveforms are shown in Fig. 4-5. In all of the simulation results, the continuous lines are

by ORCAD.



voltage and the discrete lines are current. Fig. 4(a) shows that the main switches turn off and on under zero voltage. Also ZVS of main diode can be seen in fig. 4(b). fig. 5(a) shows the auxiliary switch turn off under ZVZCS and turn on under ZCS condition. This figure shows that the auxiliary switch can turn on near ZCS because of the discharge of the parasitic drain-source capacitor. Soft switching of the auxiliary diode D_2 is shown in fig. 5(b). This figure shows the diode switching is under ZVS condition.

Fig. 6 shows the efficiency comparison of the proposed converter and dual input hard switching boost converter. This curve is plotted by simulation results of the ORCAD. Continuous line shows the efficiency of the proposed converter and discrete line shows the efficiency of the hard switching counterpart. This figure shows 1 percent improvement in efficiency of proposed converter in comparison with hard switching counterpart.

IV. CONCLUSION

In this paper, the proposed dual input ZVS converter theoretically is analyzed. And various operating mode and simulation results are investigated. Simulation results show that the proposed technique can have one percent improvement in the efficiency of the converter at the nominal load. In addition, due to using of the ZVT technique, EMI noise has decreased significantly because dv/dt has been decreased. The simulation result confirms the theoretical analysis of operation. It must be noted that, the control of this converter is PWM. And the number of required switches to provide the soft switching condition is just one switch and it can be easily improved to multi inputs. The diode reverse-recovery is solved by providing ZVS condition for main diode. The proposed converter is providing soft switching conditions with one auxiliary circuit for all semiconductor elements. Suggested idea

can easily expanded for more boost converter that is one of the strong points of this technique.

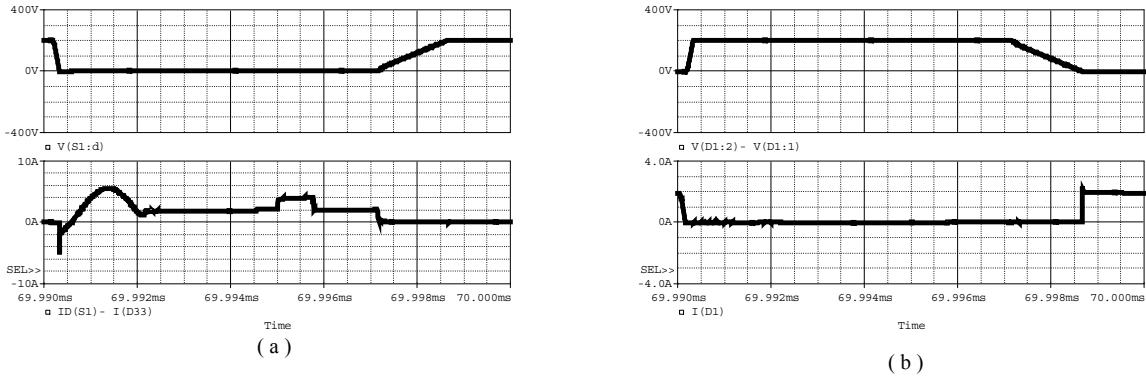


Figure 4. (a)voltage and current waveform of the main switch (b)voltage and current waveform main diode

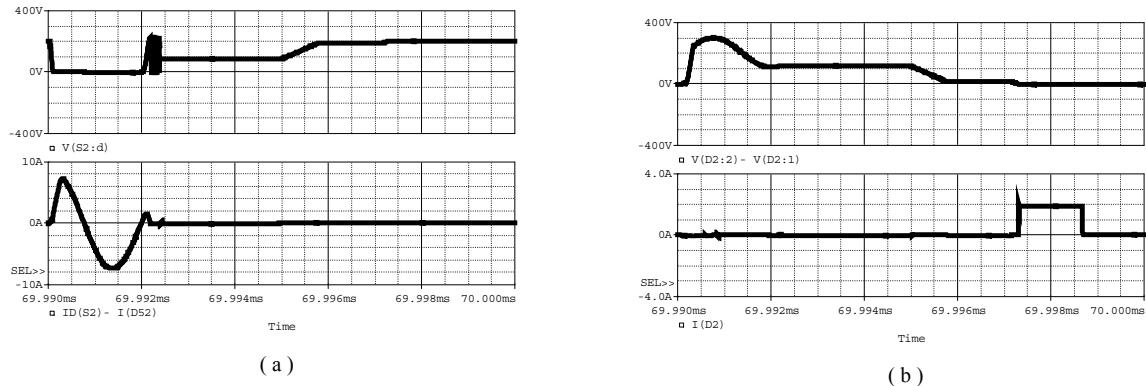


Figure 5. (a)voltage and current waveform of the auxiliary switch (b)voltage and current waveform auxiliary diode

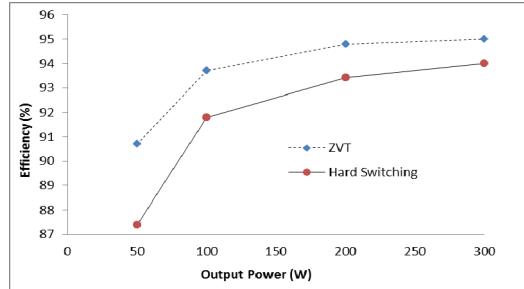


Figure 6. Efficiency comparison of the proposed converter and dual input hard switching boost converter

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